

4.6 Laser Oscillation Conditions

A. Optical Gain Coefficient, g

- Propagating em-wave in a laser medium along x -direction.

Optical gain coefficient of the medium, g

$g \rightarrow$ fractional change in the light power (or intensity) per unit distance.

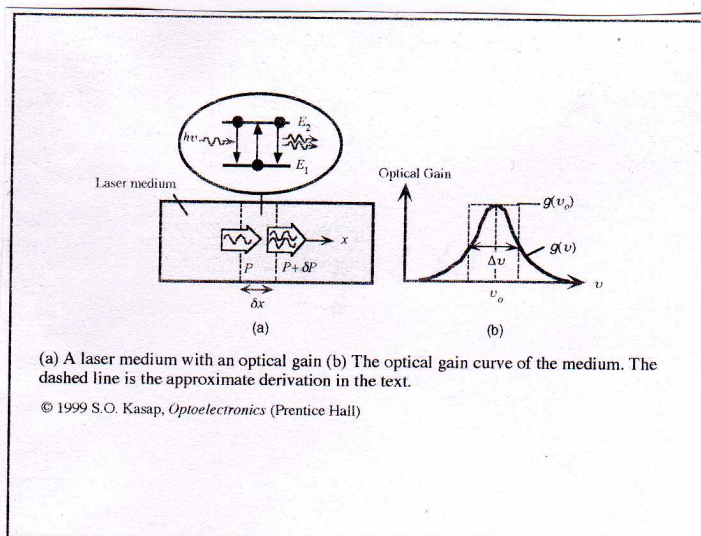
Optical power P is proportional with the concn. of coherent photons, N_{ph} and their energies, $h\nu$.

The photons travel a distance $\left[\delta x = \frac{c}{n} \delta t \right]$ in the medium.

$$\therefore g = \frac{\delta P}{P} \frac{1}{\delta x} = \frac{\delta N_{ph}}{N_{ph} \cdot \delta x} = \frac{n}{c N_{ph}} \frac{\delta N_{ph}}{\delta t}$$

\rightarrow The net rate of change in coherent photon concentration:

$$\begin{aligned} \frac{dN_{ph}}{dt} &= \text{Net rate of stimulated photon emission} \\ &= N_2 B_{21} \rho(h\nu) - N_1 B_{12} \rho(h\nu) \\ &= (N_2 - N_1) B_{21} \rho(h\nu) \end{aligned}$$



Emission is within $\Delta\nu$ interval (eg. due to Doppler broadening)

$\therefore g = g(\nu)$

$\therefore \rho(h\nu) \rightarrow$ energy density per unit freq.

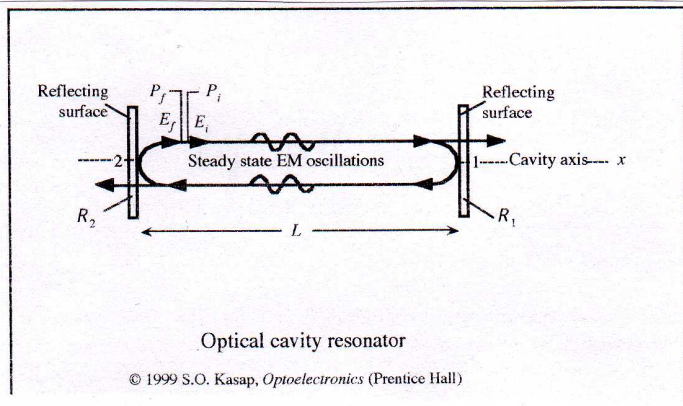
$$\rho(h\nu_0) \approx \frac{N_{ph} h\nu_0}{\Delta\nu}$$

Gain Coefficient:

$$g(\nu_0) \approx (N_2 - N_1) \frac{\beta_{21} n h\nu_0}{c \cdot \Delta\nu}$$

optical gain at ν_0

B. Threshold Gain g_{th}



The net round-trip optical gain

G_{op} must be unity (\equiv no gain and no loss)

$$G_{op} = \frac{P_f}{P_i} = 1$$

$$P_f = P_i R_1 R_2 \exp[g(2L)] \exp[-\gamma(2L)]$$

Attenuation or loss coeff. of the medium and represents all losses in the cavity and the walls except transmission losses from mirrors.

In steady state $G_{op} = \frac{P_o}{P_i} = 1$ must be satisfied.

The value of g that makes this eq. is valid is called **threshold gain g_{th}** .

$$g_{th} = \gamma + \frac{1}{2L} \ln\left(\frac{1}{R_1 R_2}\right)$$

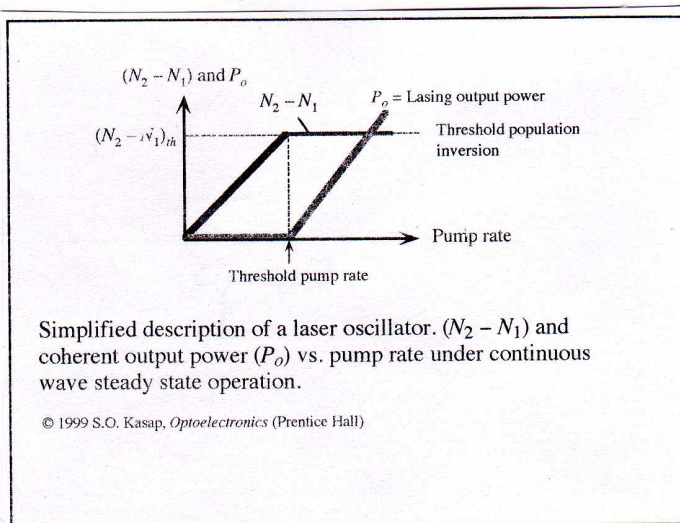
→ The necessary g_{th} has to be obtained by suitably pumping so that $N_2 \gg N_1$.

Threshold population inversion $\rightarrow N_2 - N_1 = (N_2 - N_1)_{th}$:

$$(N_2 - N_1)_{th} \approx g_{th} \cdot \frac{c \Delta V}{B_{21} n h \nu_0^2}$$

→ Initially the medium must have a gain coefficient g greater than g_{th} .

→ When the steady state is reached, $\therefore g = g_{th}$ $g > g_{th}$



→ Until the pump rate can bring $(N_2 - N_1)$ to $(N_2 - N_1)_{th}$, **no coherent radiation.**

→ When the pumping rate exceeds the threshold, $(N_2 - N_1)$ remains clamped at $(N_2 - N_1)_{th}$.

→ Additional increase in pumping increases the rate of stimulated transitions and \therefore the optical output power P_o .

C. Phase Condition and Laser Modes

4.44.

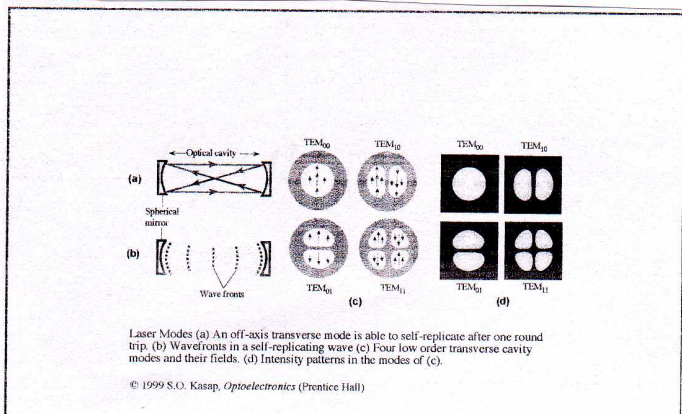
After one round-trip the phase-change $\Delta\phi_{\text{round-trip}}$

$$\Delta\phi_{\text{round-trip}} = m(2\pi)$$

$$nk_m(2L) = m(2\pi)$$

Mode condition \rightarrow

$$m \left(\frac{\lambda_m}{2n} \right) = L$$



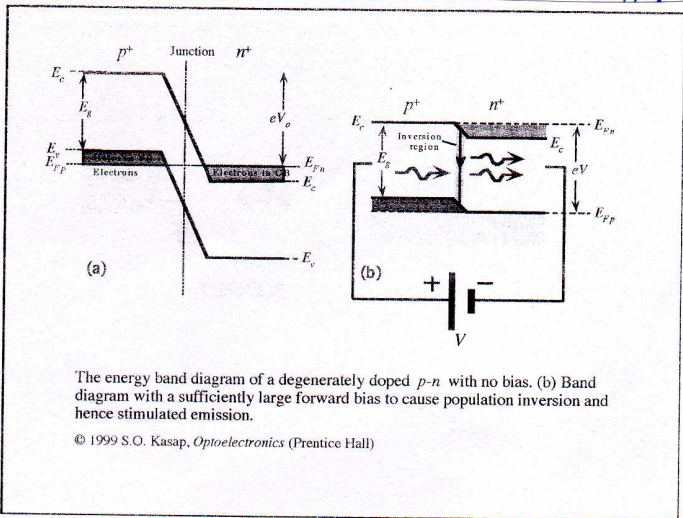
Transverse modes or Transverse Electromagnetic Modes TEM_{pqm}

TEM_{pqm}

The number of nodes in the field distribution along transverse directions
 The number of nodes along the cavity axis and generally NOT shown.
 ($m \sim 10^6$ for gas lasers)

4.7. Principle of the Laser Diode

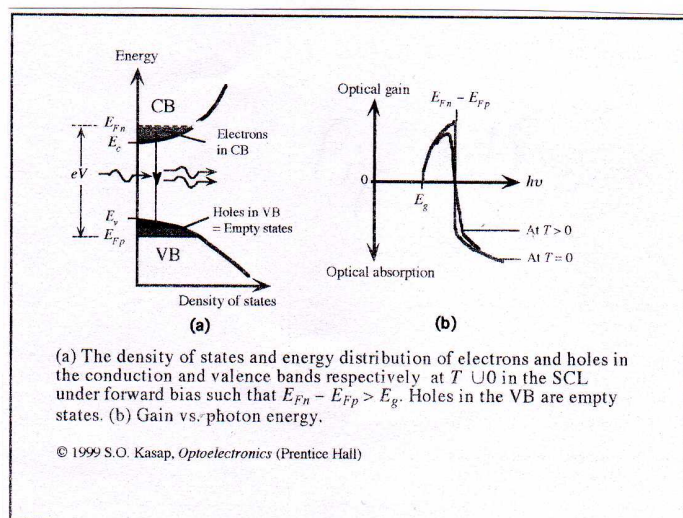
Degenerately doped direct band gap s/c pn junction



→ Very narrow depletion region.

→ Population inversion (forward biased) is around the junction
Inversion layer or active region.

→ An incoming photon can NOT EXCITE an electron, \because ^{the edge of} E_v is empty.
However, it can stimulate an electron to fall down.

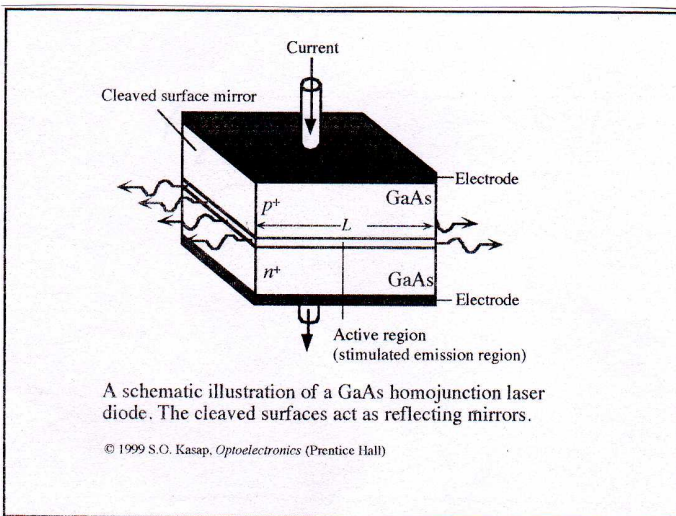


→ Photons have energies greater than E_g but less than $(E_{Fn} - E_{Fp})$

→ As T increases (from $T \approx 0$), F.D. spreads the elec. energies.
 \therefore a reduction in optical gain

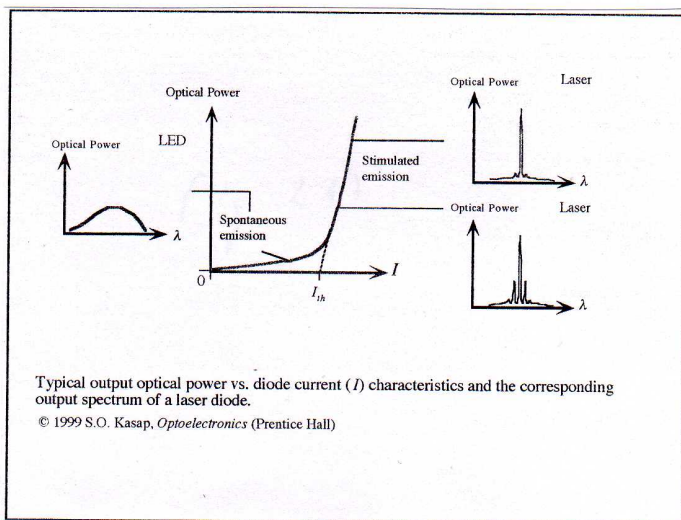
→ The pumping mechanism is ∴ the forward diode current and pumping energy is supplied by the external battery.
 This type of injection is **INJECTION PUMPING**

Besides population inversion, we need to have an **OPTICAL CAVITY**



$$m = \frac{2L}{\lambda} = 2n$$

Modes in an optical cavity



- When $I < I_{th}$
Spontaneous emission
- When $I > I_{th}$
Stimulated emission.

→ Transparency current is the diode current providing just enough current to inject electrons to balance the absorption.
 No net photon absorption \Rightarrow the medium is transparent

→ The main problem with the homojunction laser diode is

J_{th} is so large that it's in the order of $\sim 500 \text{ A/mm}^2$ for GaAs

→ HOWEVER, J_{th} can be reduced by orders of magnitude by using heterojunctions &c diodes.

4.8. Heterostructure Laser Diodes.

To reduce J_{th} → improve the rate of stimulated emission.
 and improve the efficiency of optical cavity.

→ Confine the electrons and holes to a narrow region → narrow active region.

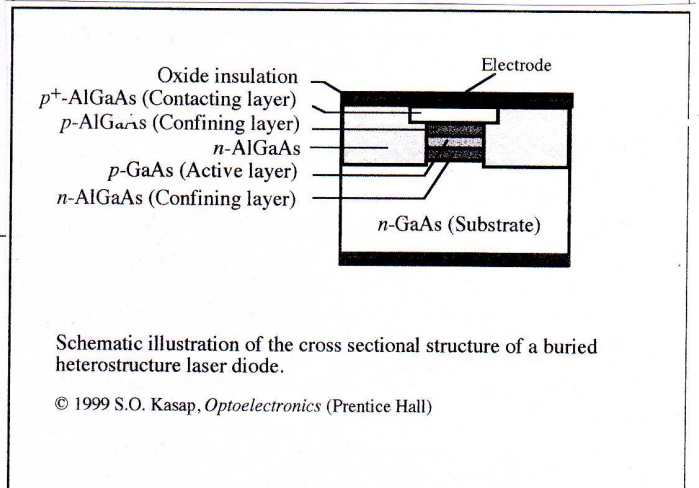
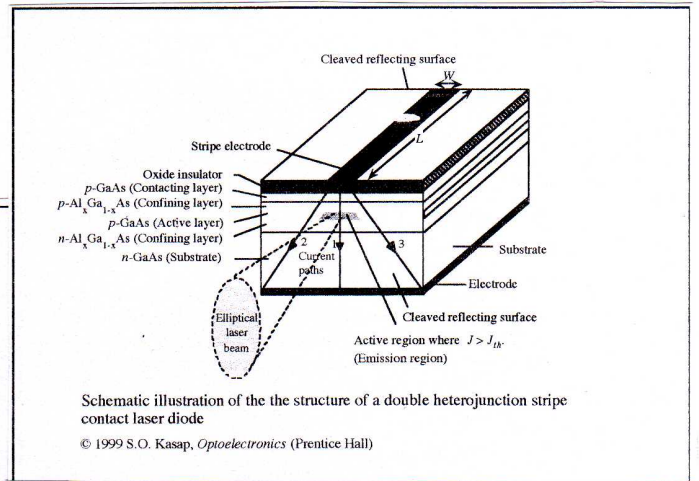
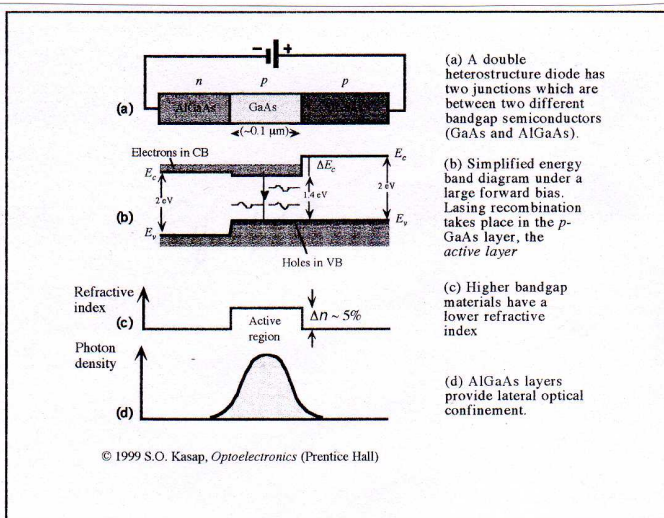
∴ less current is needed for population inversion.

→ Build a dielectric waveguide around active region.

∴ increase the photon concentration and hence prob. of stimem.

∴ We need both

- photon confinement and
- carrier confinement.



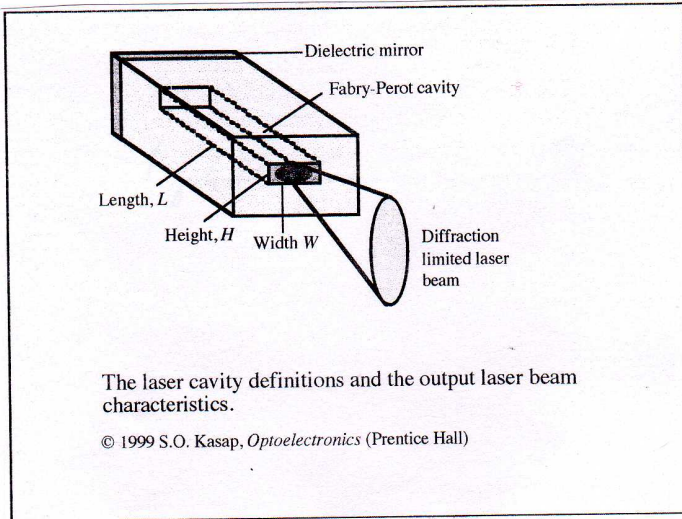
4.9. Elementary Laser Diode Characteristics

Fabry-Perot Cavity

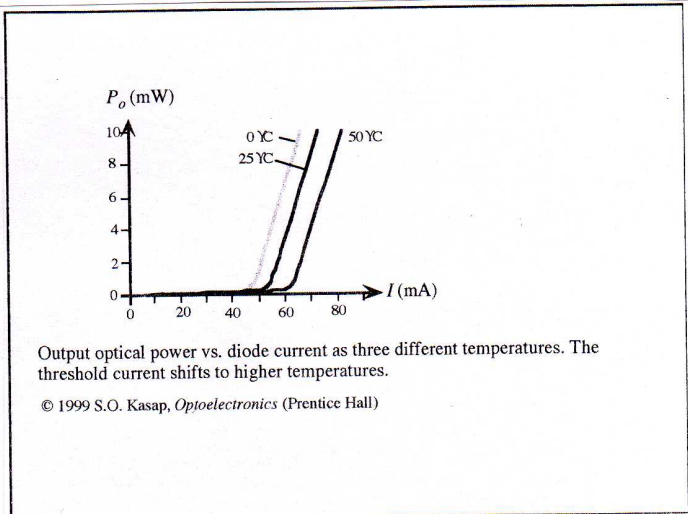
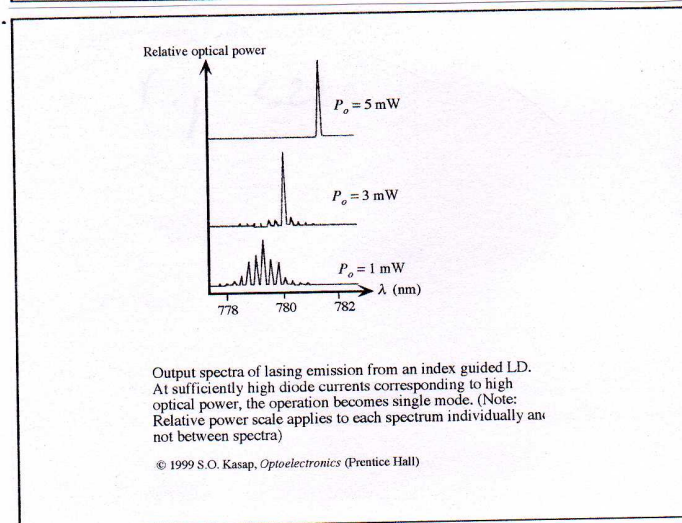
Length \leftrightarrow Longitudinal modes

Width and Height \rightarrow Transverse or Lateral modes.

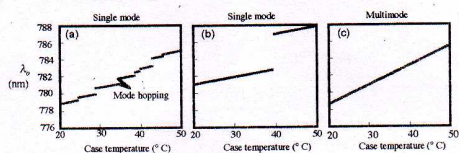
\rightarrow Sufficiently small W and $H \rightarrow$ TEM₀₀ (it has long. modes.)



- At low power outputs
LD \rightarrow single mode
- At high power outputs
LD \rightarrow Multi mode



\rightarrow As the temp. increases, threshold current increases steeply.



Peak wavelength vs. case temperature characteristics. (a) Mode hops in the output spectrum of a single mode LD. (b) Restricted mode hops and none over the temperature range of interest (20 - 40 °C). (c) Output spectrum from a multimode LD.

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→ Mode Hop → As the temp. rises, another laser mode fulfills the oscillator conditions → Due to the slight increase in n and cavity length.

→ Undesirable Mode hops → Sufficiently separated modes by changing structure

→ A gain guided laser → many modes

Highly stabilized lasers with TE coolers \approx controlling the device temp.

Slope Efficiency; Optical power output in terms of diode current

$$\eta_{\text{slope}} = \frac{P_o}{I - I_{th}}$$

4.11 Light Emitters for Optical Fiber Communications

→ For short haul applications (local networks etc.) → LEDs.

with multimode and graded index fibers. ∴ Δn is not a major concern.

LEDs;

- are simpler to drive
- more economic
- have longer lifetime
- provide necessary output power

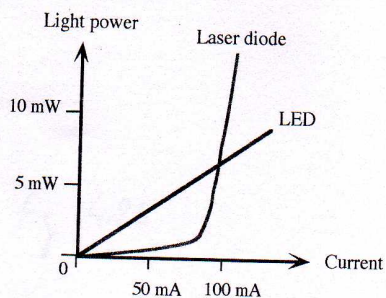
LEDs

- are typically used with multimode and graded index fibers.
- ∴ the dispersion is not major concern for these fibers.

→ For long haul and wide bandwidth communications → Laser Diodes.

∴ of their narrower bandwidth and higher output power.

Allowing only one mode → Single mode laser with a bandwidth of 0.01-0.1 nm.



Typical optical power output vs. forward current for a LED and a laser diode.

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TABLE 4.1 Typical characteristics of LEDs and Laser diodes for 1.3 μm emission. Rise time is the time it takes for the output optical power to rise from 10% to 90% in response to a step current input.

	LED	Laser diode
Structure	Double heterojunction	Double heterojunction
Material	InGaAsP on InP	InGaAsP on InP
Output radiation	Incoherent (Spontaneous emission)	Coherent (Stimulated emission)
Typical spectral linewidth, $\Delta\lambda$	100 nm	2-4 nm (multimode laser) < 0.1 nm (single mode laser)
Rise time	5-20 ns	< 1 ns

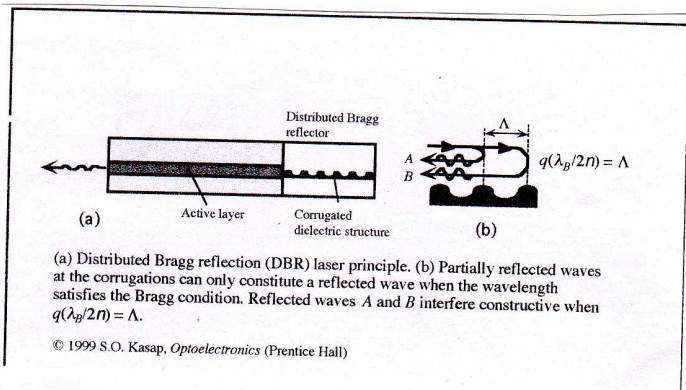
Rise time

→ The time it takes the output power to rise from 10% to 90%, when a current driving is applied suddenly as a step.

LDs have shorter rise times than LEDs.

4.12. Single frequency Solid State Lasers

One method of ensuring a single mode radiation \leftrightarrow DBR



Optical path difference $\rightarrow 2\Delta$

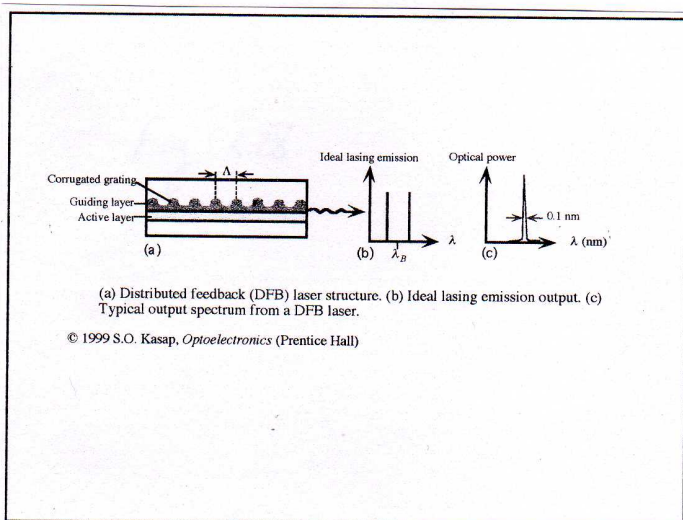
Δ is corrugation period

Diffraction order

$$q \frac{\lambda_B}{n} = 2\Delta$$

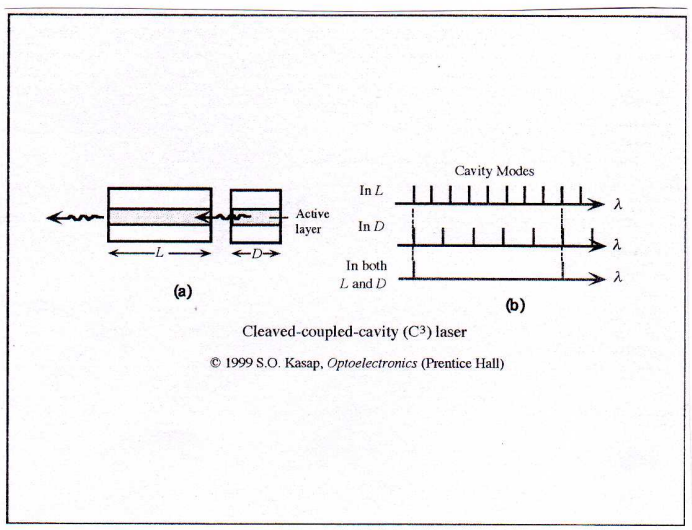
Ref. index of corrugated met.

DFB (Distributed Feedback Lasers)



Cleaved Coupled Cavity (C³) Laser

Two different laser optical cavities L and D are coupled.



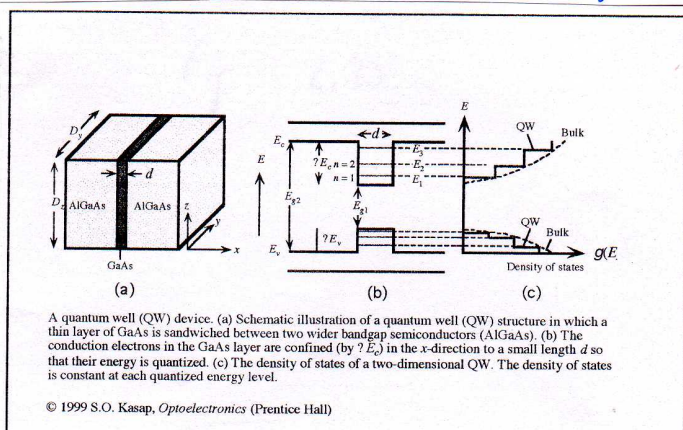
- Two levels are pumped by different currents
- Two different sets of modes coincide only at far spaced intervals!

4.13. Quantum Well Devices

A typical Q.W. device has an ultra-thin (less than 50nm) narrow band-gap semiconductor, such as GaAs, sandwiched between two wider band-gap s/c.

- lattice match is required.
- Because of pot-en. barrier, ΔE_c , conduction electrons in GaAs are confined in x -direction.

The Confinement can be treated as in 1-D, due to narrow GaAs layer. (2D electron gas)



The energy in Q.W

$$E = E_c + \frac{\hbar^2 n_x^2}{8m_e^* d^2} + \frac{\hbar^2 n_y^2}{8m_e^* D_y^2} + \frac{\hbar^2 n_z^2}{8m_e^* D_z^2}$$

n_x, n_y and n_z are Q numbers

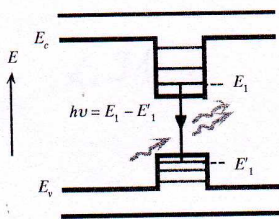
$D_y, D_z \gg d$, E_1 is associated with " d "

→ A large concentration of electrons occurs at E_1 , while almost no electronic states at E_c for a BULK s/c.

∴ population inversion, with a small current is reached between E_1 and E_2

→ Two distinct advantages of single quantum well (SQW) laser

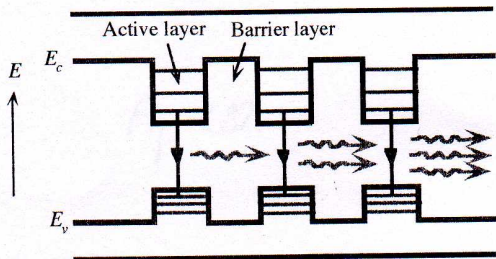
- The threshold current for population inversion is markedly reduced.
- The majority of electrons are at E_1 and holes are at E_1' , the range of emitted photon energies are very close to $(E_1 - E_1')$



In single quantum well (SQW) lasers electrons are injected by the forward current into the thin GaAs layer which serves as the active layer. Population inversion between E_1 and E_1' is reached even with a small forward current which results in stimulated emissions.

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Multiple Q.W. lasers

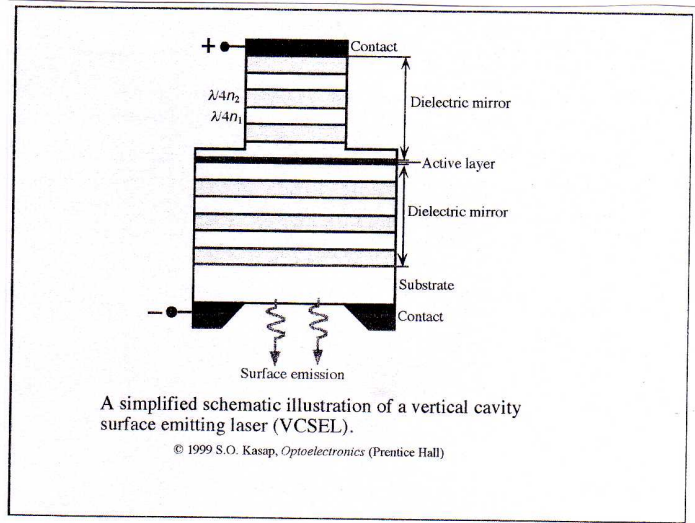


A multiple quantum well (MQW) structure. Electrons are injected by the forward current into active layers which are quantum wells.

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4.14. Vertical Cavity Surface Emitting Lasers (VCSELs)

→ The actual width is very much larger than the thickness of the active layer, then the radiation emerges from the surface.



Constructive reflections at wavelengths of λ (free space)

$$n_1 d_1 + n_2 d_2 = \frac{1}{2} \lambda$$

which leads constructive interference

instead. Phosphor contacts are used to avoid undesirable voltage drops in the DBRs.

→ High reflectance end mirrors are needed. Because the cavity length is so short that the optical gain is so small, inasmuch as the optical gain is prop. to $\exp(gL)$.

• With 20-30 layers in the DBR to obtain required reflectance 99%

• Active layers are very thin ($< 0.1 \mu\text{m}$)

For example

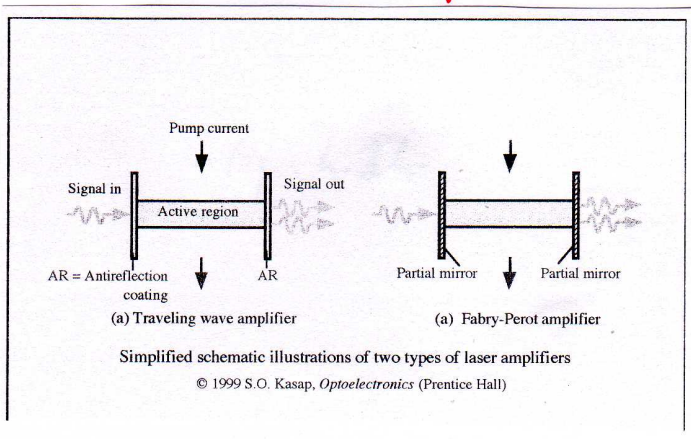
- Active layer : InGaAs as emitting at 980nm
- Substrate : GaAs transparent at 980nm
- DBR : Varying compositions of AlGaAs

The vertical cavity,

- generally circular shaped cross section, so is beam shape.
- The height of the VC may be as small as microns.
 - ∴ The longitudinal resonances are sufficiently large
- There may be ~~one~~ one or more lateral modes, depending on the lateral size of the cavity.
 - Typically less than $\sim 8\mu\text{m}$ (in diameter) → single mode.
- They can be arranged to construct a Matrix emitter.
 - The matrix emitters have a broad area as a surface emit. source.
 - They have important applications in

OPTICAL INTERCONNECT and OPTICAL COMPUTING tech.

4.15. Optical Laser Amplifiers



A-FP Amp has higher gain than T-W Amp but less stability.

A s/c laser structure can be used as an optical amplifier.

Traveling Wave s/c. laser amp.

- with AR coated at two ends of the cavity.
- However light incident on the input is amplified by **STIMULATED** emissions
- The device is pumped to achieve optical gain. (population inversion)

The Fabry-Perot laser Amp.

- similar to conventional laser osc., but operated below the threshold current.
- ∴ is not self-lasing.
- Input light is amplified by **stimulated emissions** and multiple reflections.